

Development of Low-Cost, Highly-Sinterable (Ni,Fe)₃O₄-Based Materials for SOFC Cathode-Side Contact Application

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Outline

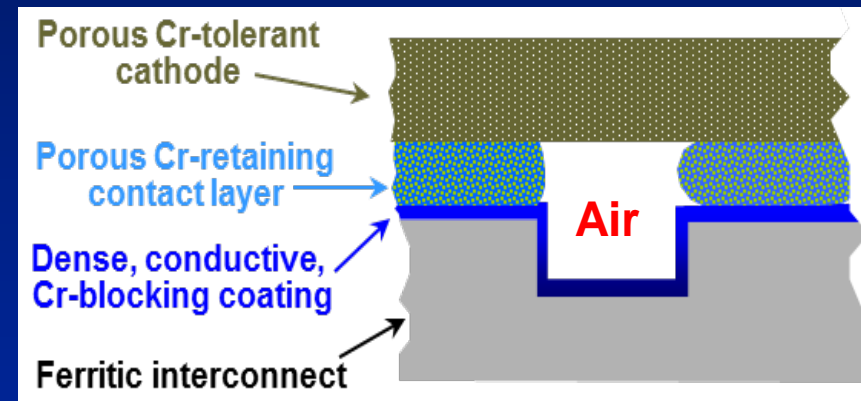
- **Introduction and Project Objectives**
- **Major Progress/Conclusions from the Phase I Study**
- **Effect of Starting Powders on the Spinel Layer Formation**
- **Performance Evaluation of the Sintered Spinel Contact**
- Area Specific Resistance (ASR), Chemical Compatibility, etc.
- **Cost Analysis**
- **Concluding Remarks**
- **Acknowledgments**

Cathode-Side Contact in SOFC Stacks

- Major functions of cathode-side contact:
 - To minimize the ohmic resistance at the interconnect-electrode interface
 - To improve mechanical bonding
 - To provide for additional gas channels to the electrode

- Requirements of cathode-side contact materials:

- Low material/processing cost
- High electrical conductivity
- Match in CTE
- Adequate stability and compatibility
- Appropriate sinterability and porosity level
- Good bonding strength with adjacent stack components

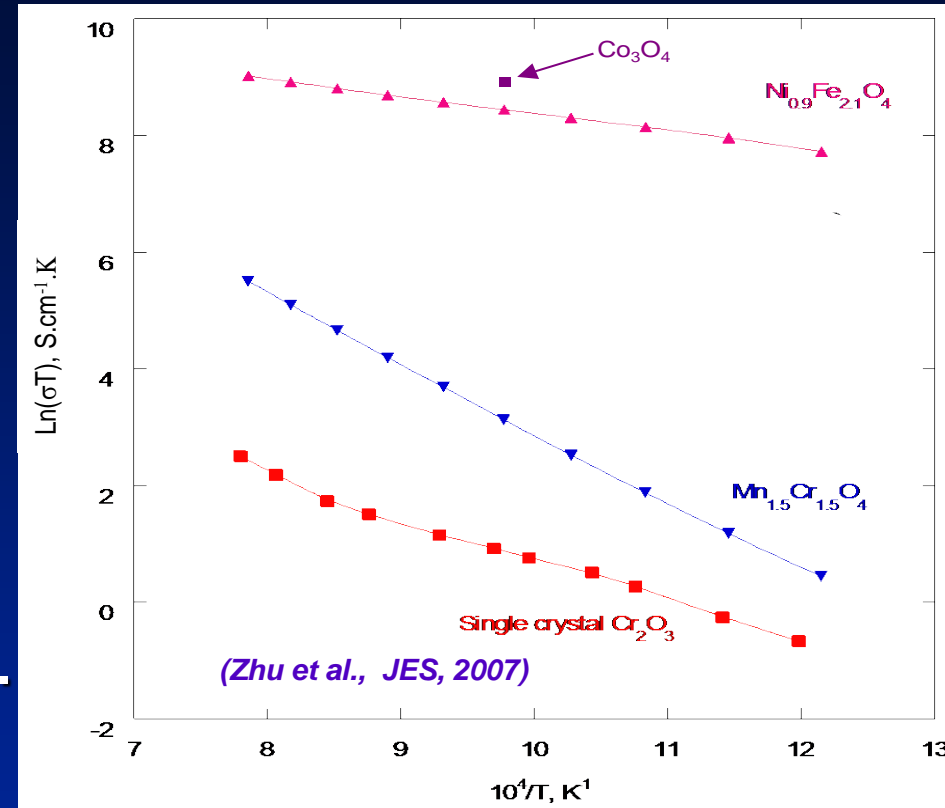


Schematic of the Cathode-Interconnect Interface

Why NiFe₂O₄-Based Spinel as Contact Material?

- Most of cathode contact developments have focused on (La,Sr)(Mn,Co,Fe,Ni)O₃:
 - Difficulty in balancing the electrical conductivity, CTE & sinterability of perovskites.
- Conductive spinels based on NiFe₂O₄ are also promising:
 - Low cost, decent electrical conductivity and CTE (12x10⁻⁶/°C).

Metal	Cost (\$/lb)
Cobalt	13.5
Nickel	4.5
Iron	0.2



Electrical Conductivity of (Ni,Fe)₃O₄, as Compared with Other Oxides

- Unfortunately, the sinterability of NiFe₂O₄ is poor (≥1200°C) if metal oxides are used. Novel sintering mechanisms need to be identified and utilized to lower its sintering temperature.

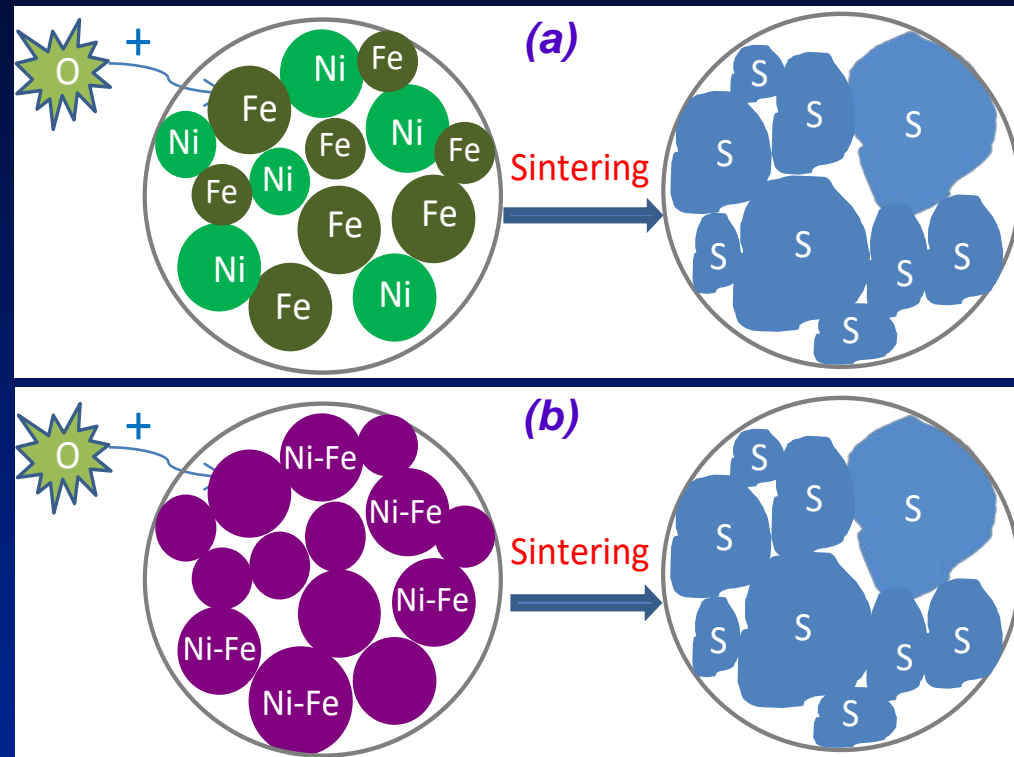
Utilization of EARS for Reduced-Temperature Sintering of (Ni,Fe)₃O₄-Base Spinel Contact

- Employment of **metallic powders** instead of oxide powders as the starting precursor to lower the sintering temperature

- Environmentally-Assisted Reactive Sintering (EARS) :



vs.

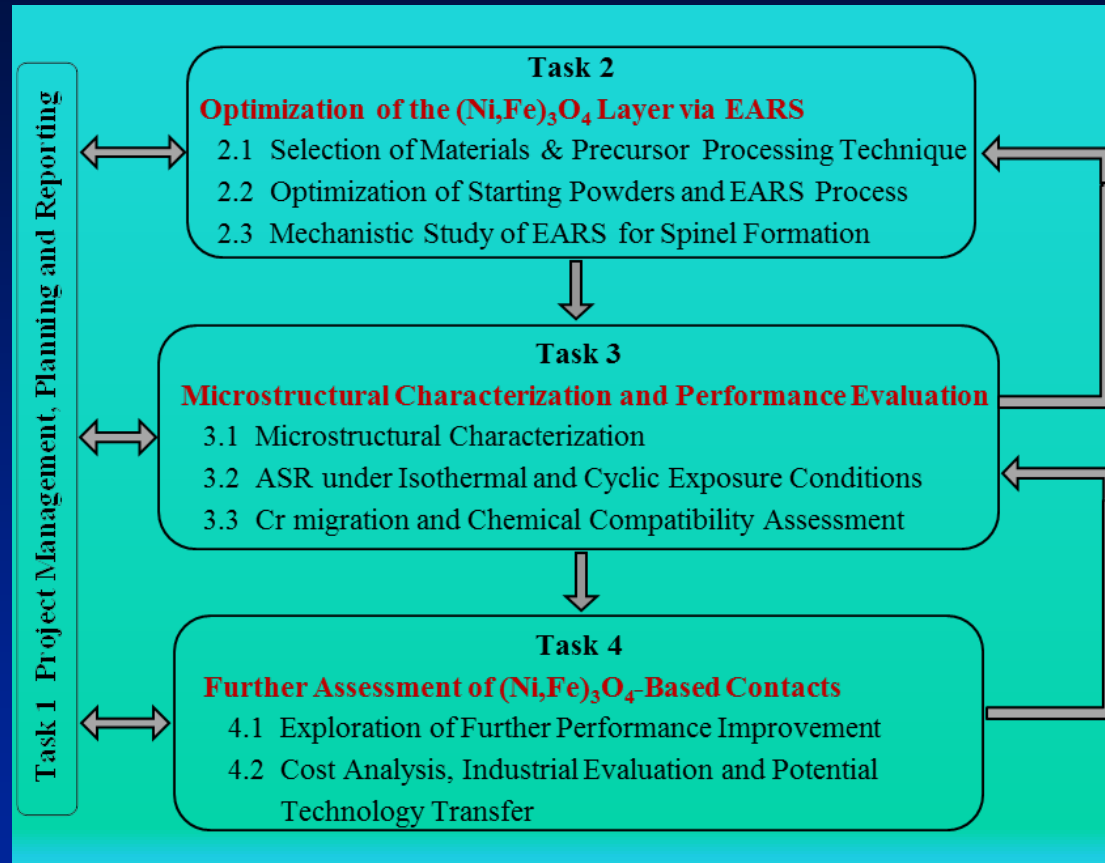


Synthesis of (Ni,Fe)₃O₄ ("S") via EARS using (a) Mixed Fe & Ni Powders; (b) Fe-Ni Alloy Powder

- Enhanced sintering via EARS due to the following facts:
 - Heat released during the reaction;
 - Volume expansion upon conversion of metal to metal oxide;
 - Formation of highly active, nanoscale surface oxides
 - Shorter diffusion distance when a prealloyed powder is employed. 5

Phase I Project Objectives

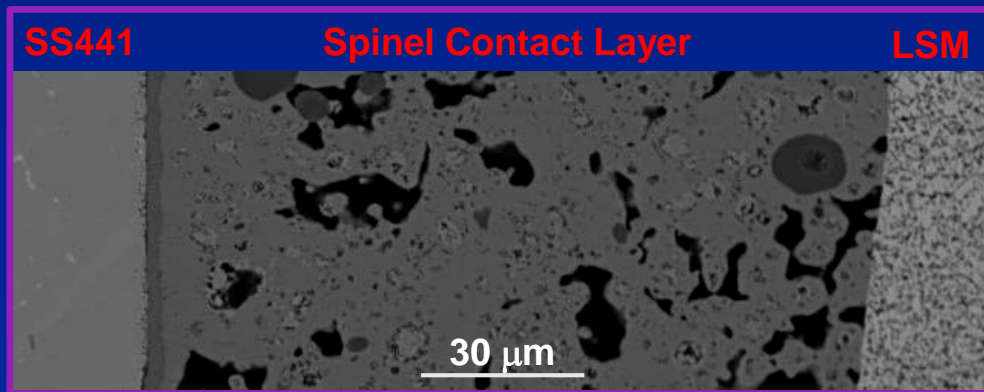
- Optimization of the $(\text{Ni,Fe})_3\text{O}_4$ spinel layer formation via controlling the parameters involved in EARS (especially the type of metallic precursors).
- Critical assessment of the performance of the EARS $(\text{Ni,Fe})_3\text{O}_4$ layer
- Exploration of further performance improvement & cost analysis



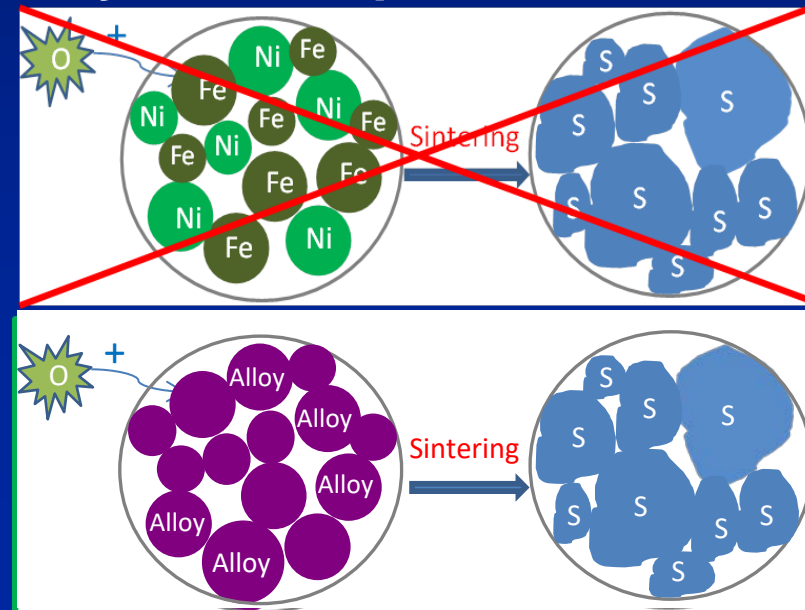
Flow Chart of the Research Tasks Involved in the Phase I Project

Major Progress/Conclusions

- A mixture of Fe + Ni powders, binary Fe-Ni or ternary Fe-Ni-Co alloy powder can be used as precursor to form a spinel layer.
- The ternary alloy powder is preferred, due to more uniform spinel conversion, better compatibility, and lower ASR.
- Approaches for further improving the performance of the spinel contact have been identified.
- A total stack cost reduction of around 6.9% can be achieved with the implementation of the new alloy contact precursor.

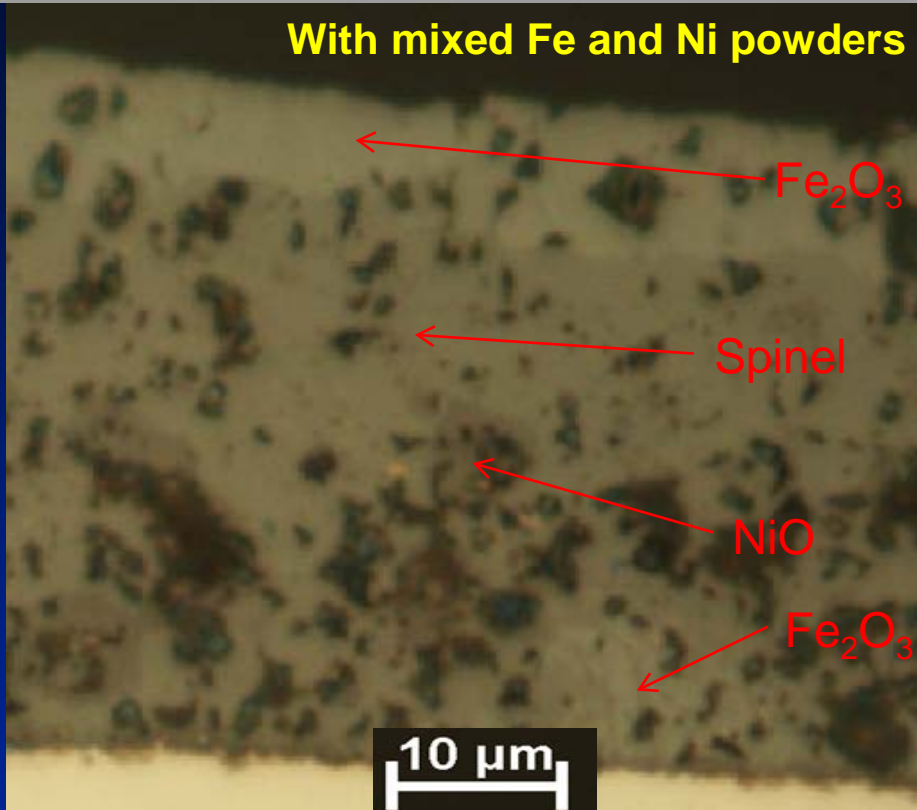


Microstructure of Test Cell with Fe-Ni-Co Alloy Precursor Contact after Thermal Exposure at 800°C for 1000 h

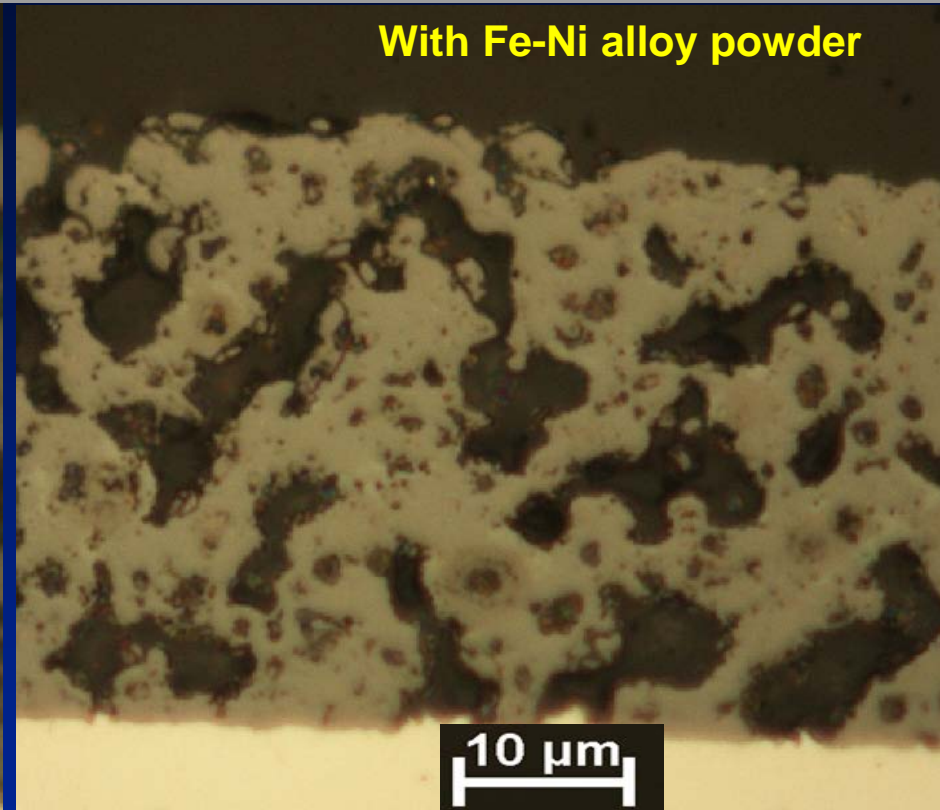


The Fe-Ni alloy powder is preferred over a mixture of Fe and Ni powders as spinel-forming precursor

With mixed Fe and Ni powders



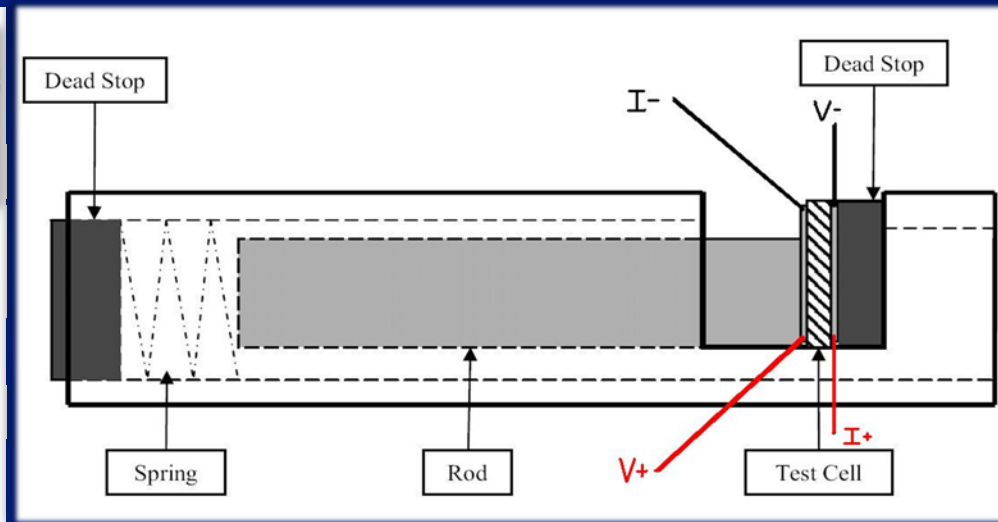
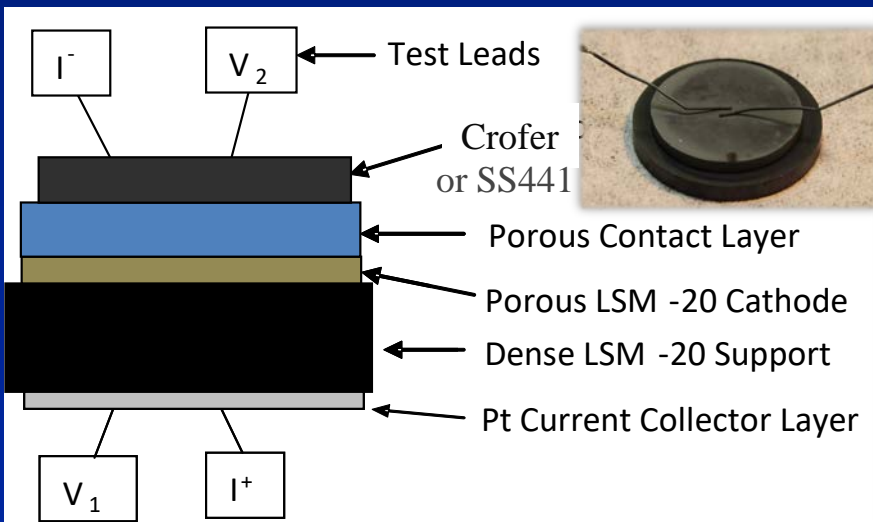
With Fe-Ni alloy powder



- With the starting powder mixture of 3- μm Fe and 2- μm Ni, the metallic layer was fully converted into an oxide layer after 900°Cx2h in air;
- A surface Fe_2O_3 sub-layer and some areas of internal NiO and Fe_2O_3 were observed, indicating a non-uniform microstructure.
- The converted spinel layer with the Fe-Ni alloy powder was relatively uniform microstructurally and compositionally.

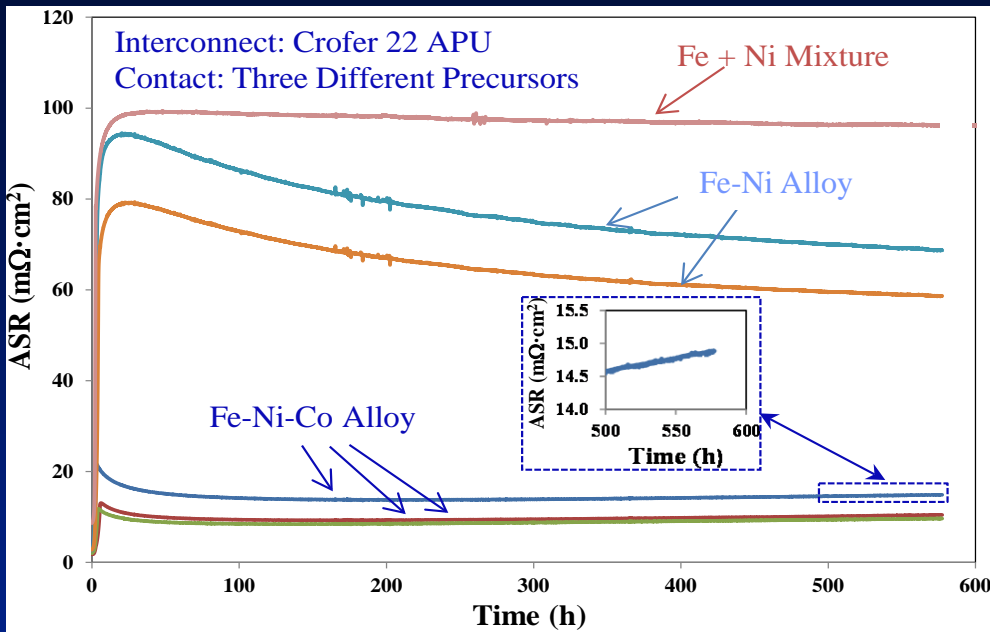
Area-Specific Resistance (ASR) Measurement

- A number of test cells were constructed, with the spinel-forming contact precursor layer sandwiched between the interconnect (Crofer 22 APU or SS 441) and the LSM cathode.
- The test cells were spring-loaded and the ASR change during either isothermal or cyclic exposure at 800°C in air was monitored using a special 6-cell test rig.

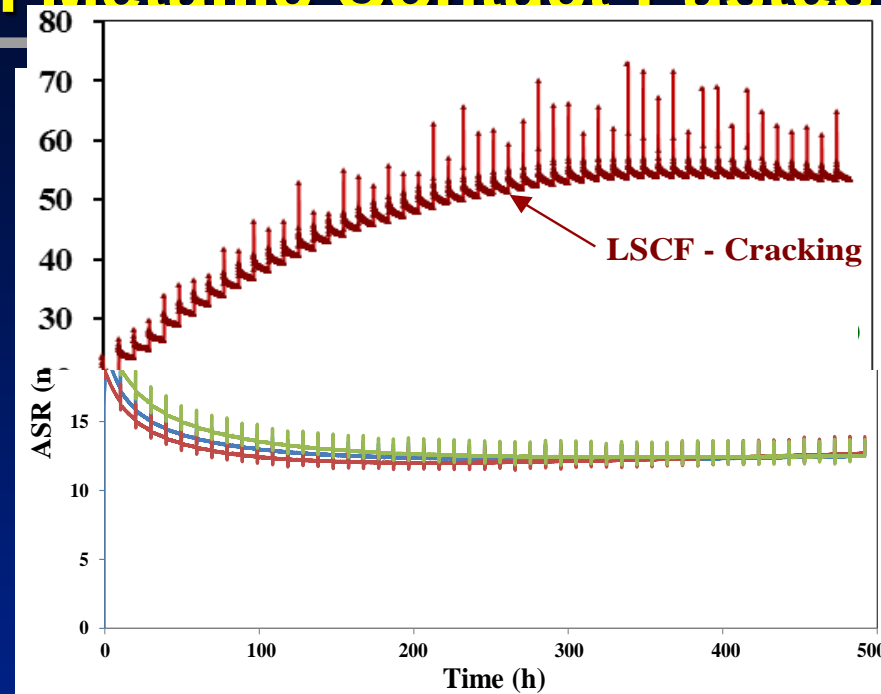


Schematic of the ASR Test Cell and Test Configuration

ASR Change as a Function of Time for Crofer 22 APU/Contact/LSM Cells with Metallic Contact Pastes



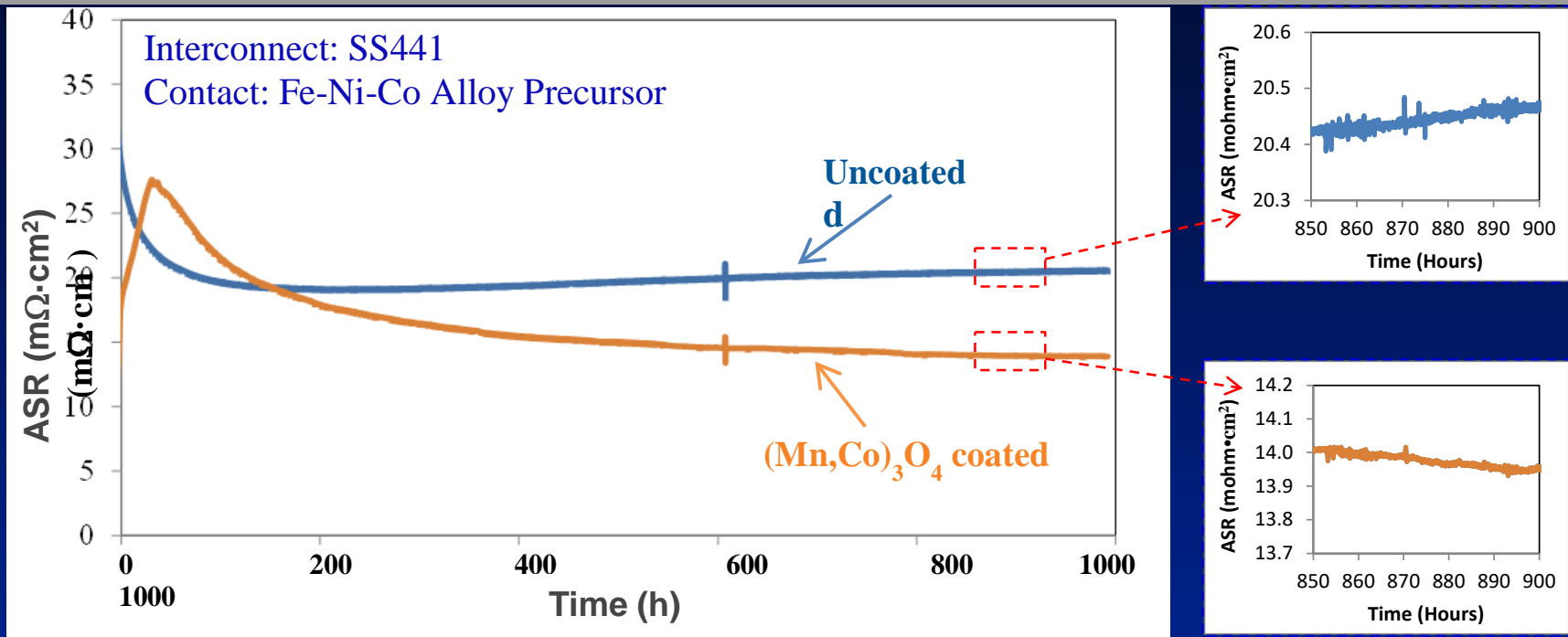
Cell ASR at 800°C during Isothermal Exposure of Test Cells with Various Contact Precursors



Cell ASR at 800°C during Cyclic Exposure of Test Cells with Ternary Alloy Precursor

- During isothermal exposure, the ASR for test cells with the mixed Fe+Ni precursor were higher than those with the alloy precursors, and the cell with the Fe-Ni-Co alloy precursor exhibited the lowest ASR.
- Thermal cycling had minimal effect on the ASR performance for test cells with the Fe-Ni-Co alloy contact precursor, due to the excellent CTE match of the contact layer with adjacent stack components.

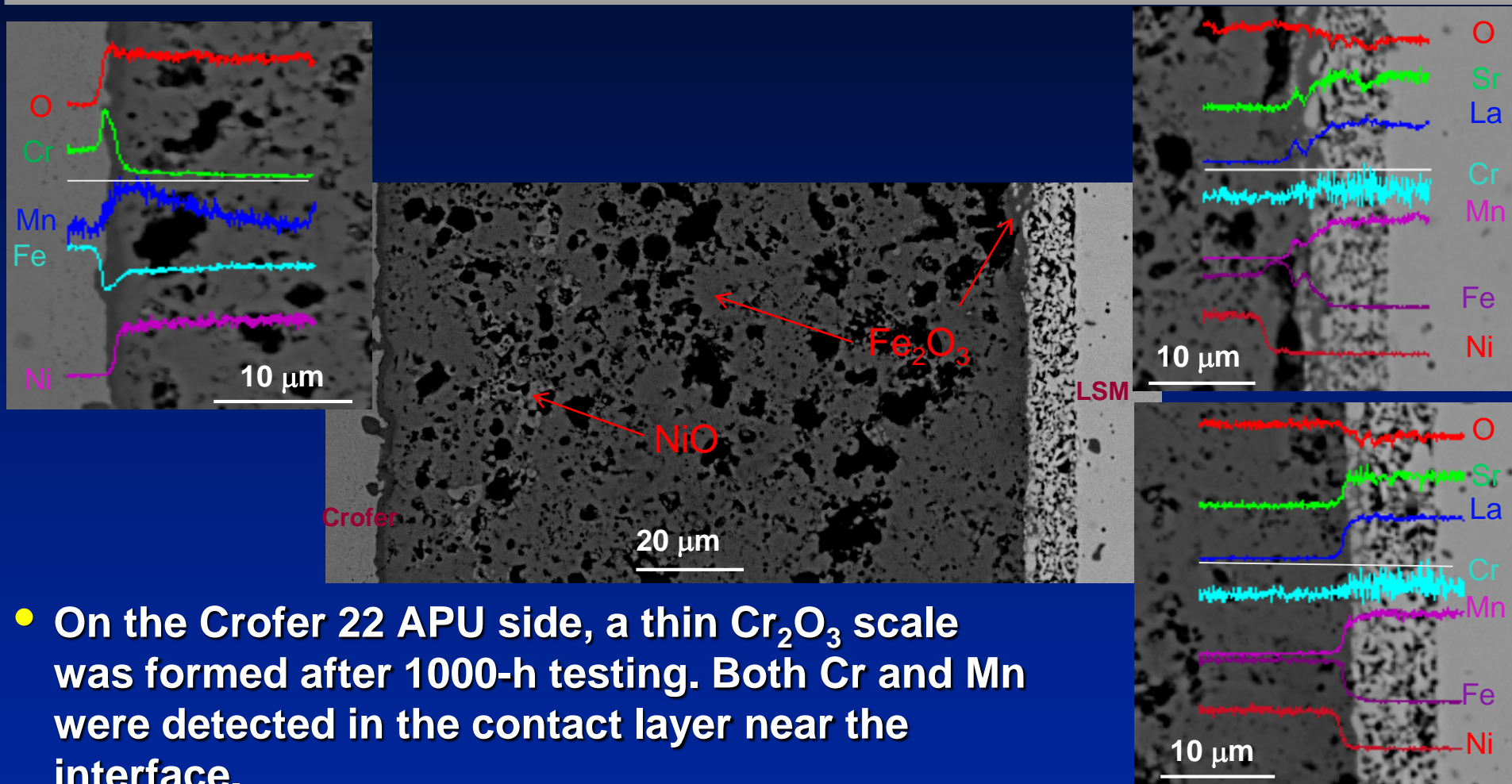
Effect of Spinel-Based Interconnect Coating on the ASR Performance of SS 441/Fe-Ni-Co Contact/LSM Cells



ASR vs. Time during 1000-h Isothermal Testing at 800°C in Air for Test Cells with Uncoated and $(\text{Mn,Co})_3\text{O}_4$ -Coated SS 441 Interconnects

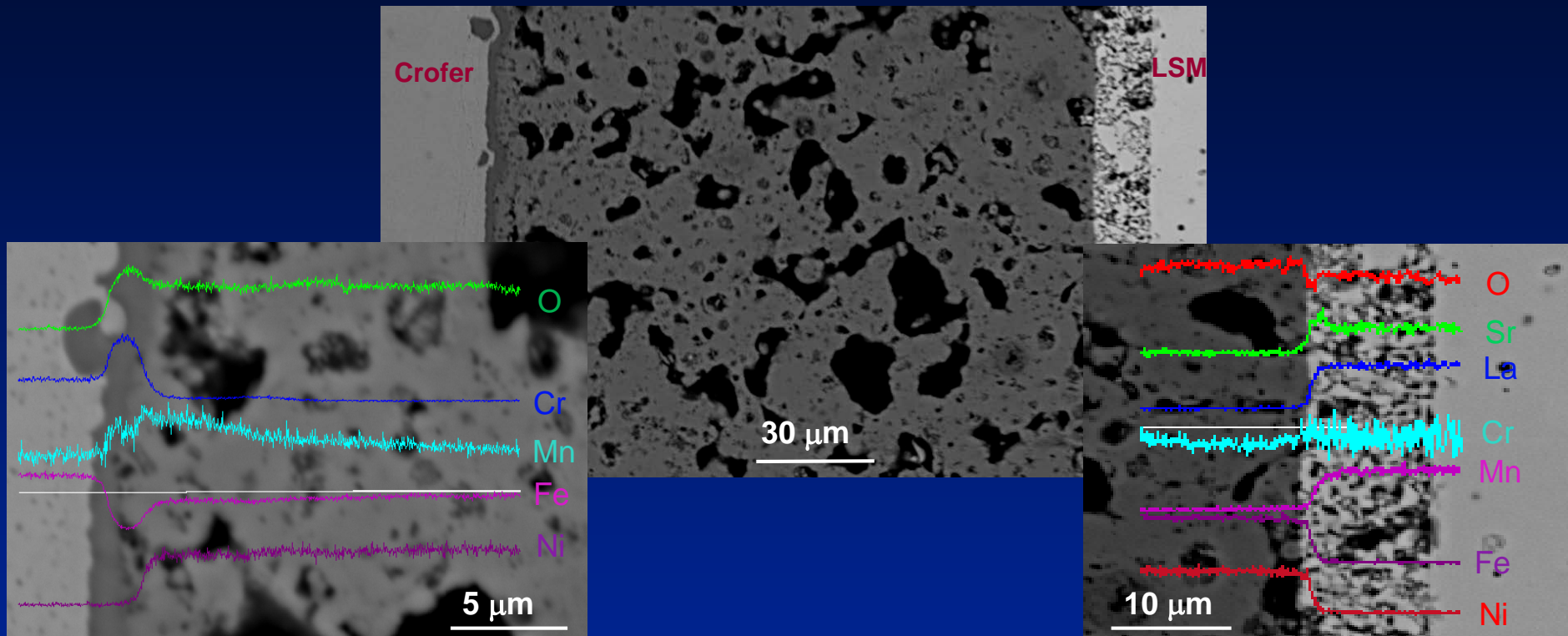
- With SS 441 as interconnect, the cell ASR was $\sim 20 \text{ m}\Omega\cdot\text{cm}^2$ and increased at a low rate, similar to the results with Crofer 22 APU as interconnect.
- However, with application of an EARS-processed, Ce-modified $(\text{Mn,Co})_3\text{O}_4$ coating on SS 441, the cell ASR continued to drop during the test.
- The overall promising ASR performance of interconnect/contact/LSM cells with the ternary alloy as the contact precursor was further confirmed.

Cross-Section of Crofer 22 APU/Contact/LSM Cells with a Mixture of Fe+Ni Powders as Contact Precursor



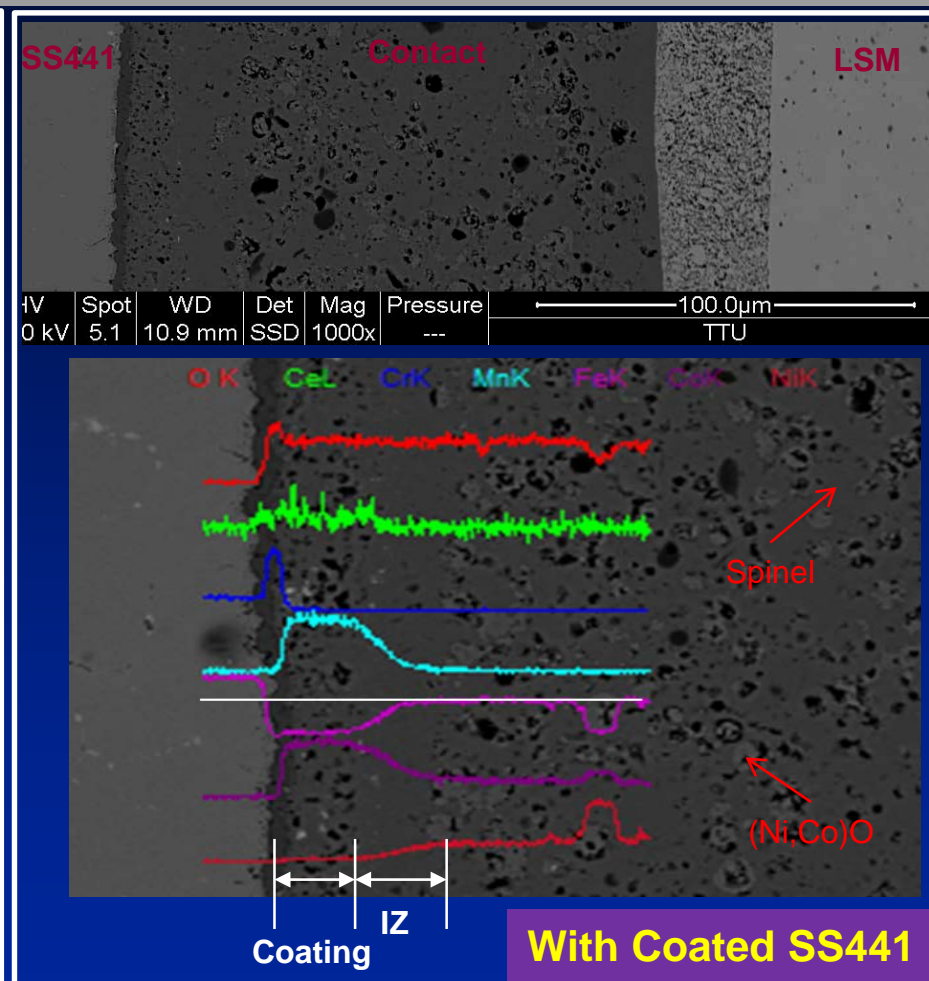
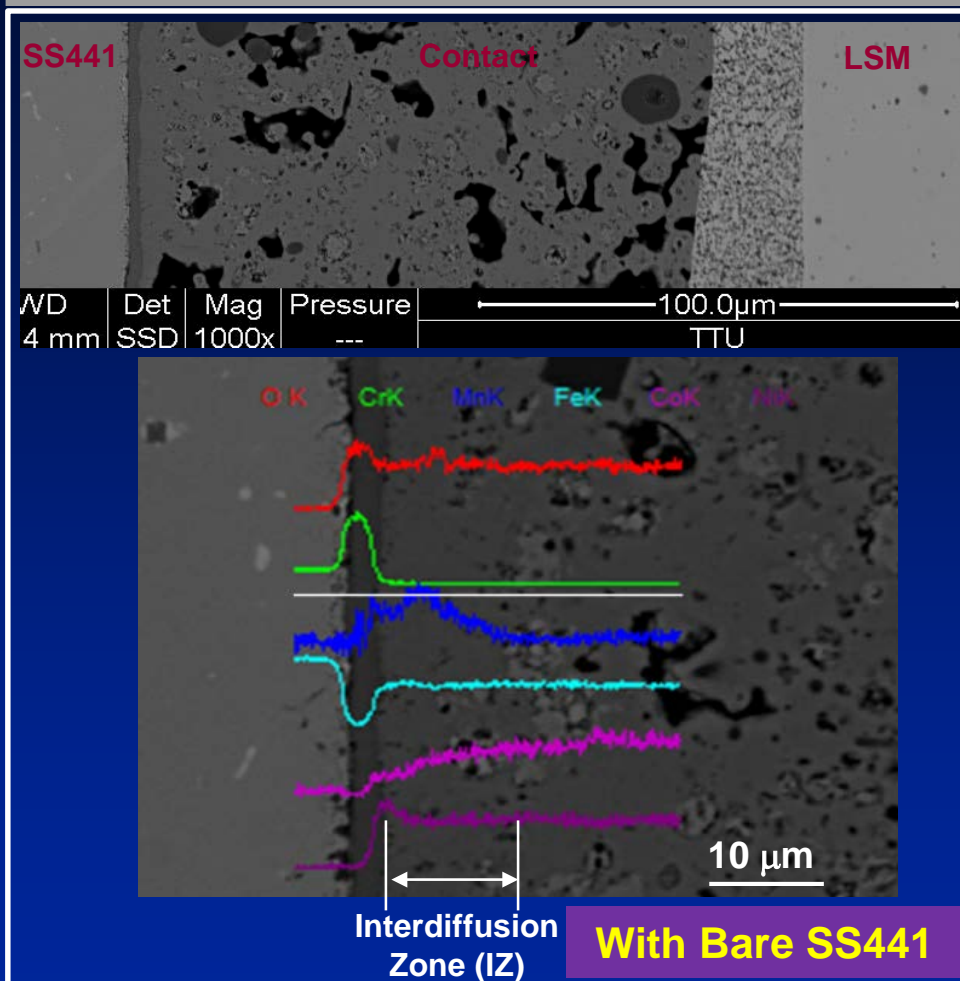
- On the Crofer 22 APU side, a thin Cr₂O₃ scale was formed after 1000-h testing. Both Cr and Mn were detected in the contact layer near the interface.
- The Fe+Ni contact layer was less uniform compositionally and structurally near the cathode-contact interface. Fe₂O₃ penetration into the cathode observed in some areas.

Cross-Section of Crofer 22 APU/Contact/LSM Cells with the Fe-Ni Alloy Contact Paste



- On the Crofer 22 APU side, a thin Cr_2O_3 scale was formed after 1000-h testing and both Cr and Mn were detected in the contact layer near the interface.
- On the cathode side, negligible interdiffusion between the contact layer and LSM was observed. No Cr was detected in LSM.

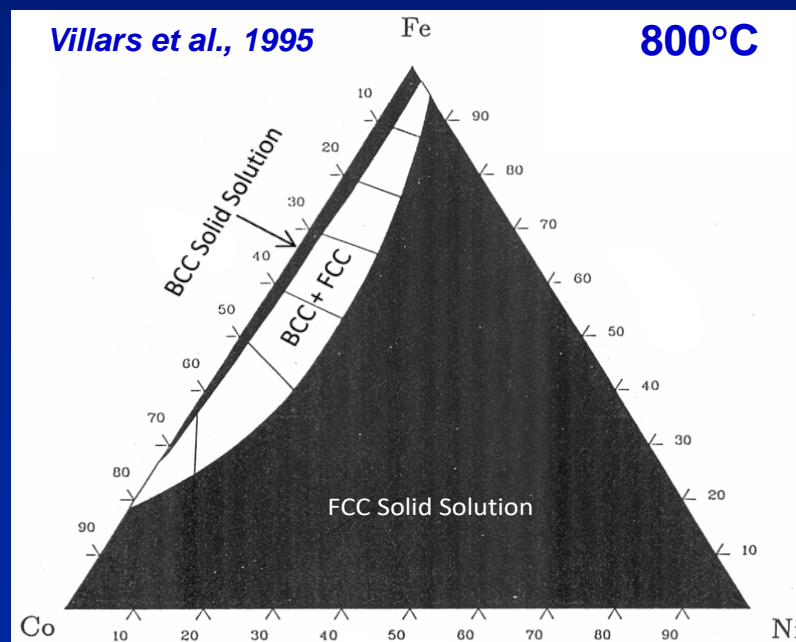
Cross-Sectional Views of SS441/Contact/LSM Cells with the Fe-Ni-Co Alloy Contact Precursor



- A thicker Cr_2O_3 scale and a larger interdiffusion zone (IZ) were formed between SS441 and the contact layer for the cell with the bare (uncoated) interconnect.
- The application of the spinel coating on the interconnect alloy significantly reduced the interdiffusion between the interconnect and the contact layer.

Further Improvement of NiFe_2O_4 -Based Spinel Contact: Alloy Design Approach

- The alloy composition can be optimized via a combination of fundamental study of phase equilibria & composition screening in the Fe_2O_3 -NiO- Co_3O_4 system, alloy design using physical metallurgy principles, and cost considerations.
 - ✓ Optimization of the Fe/Ni/Co levels
 - ✓ Addition of microalloying elements
 - ✓ Powder fabrication and characterization

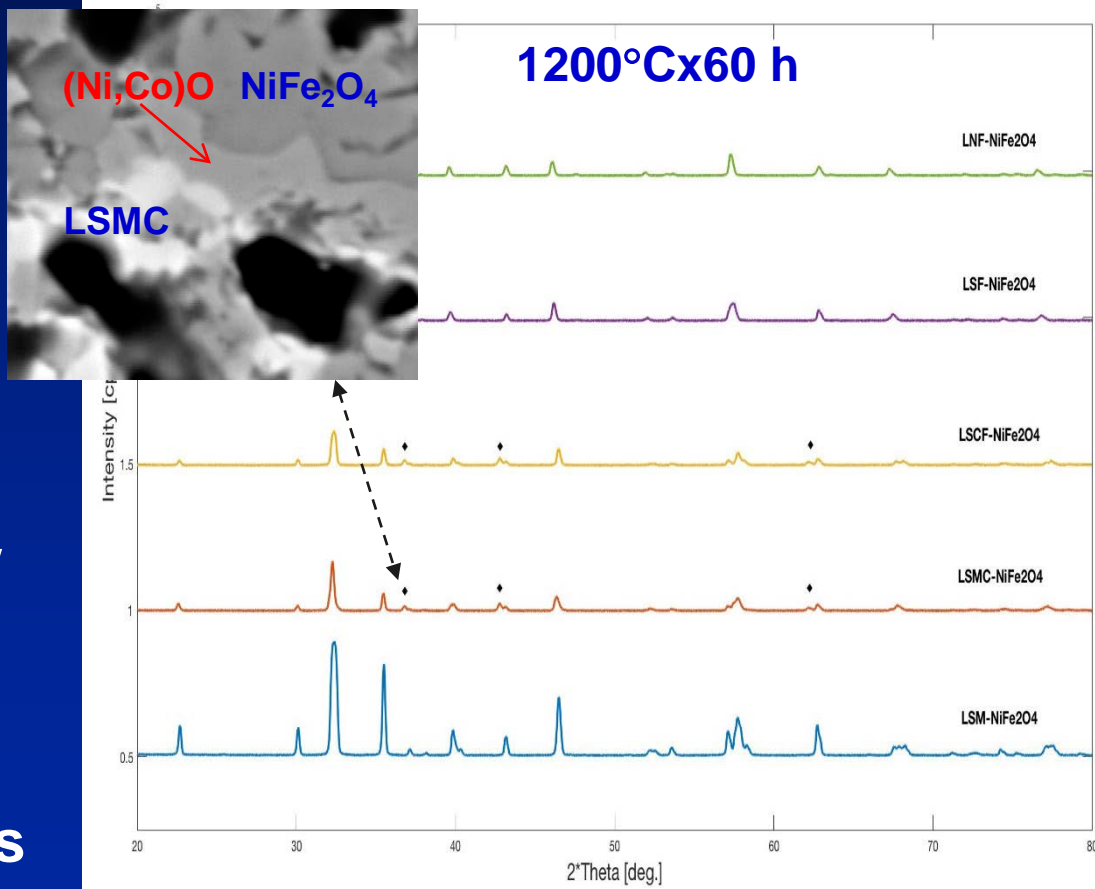


Ternary Fe-Ni-Co Phase Diagram

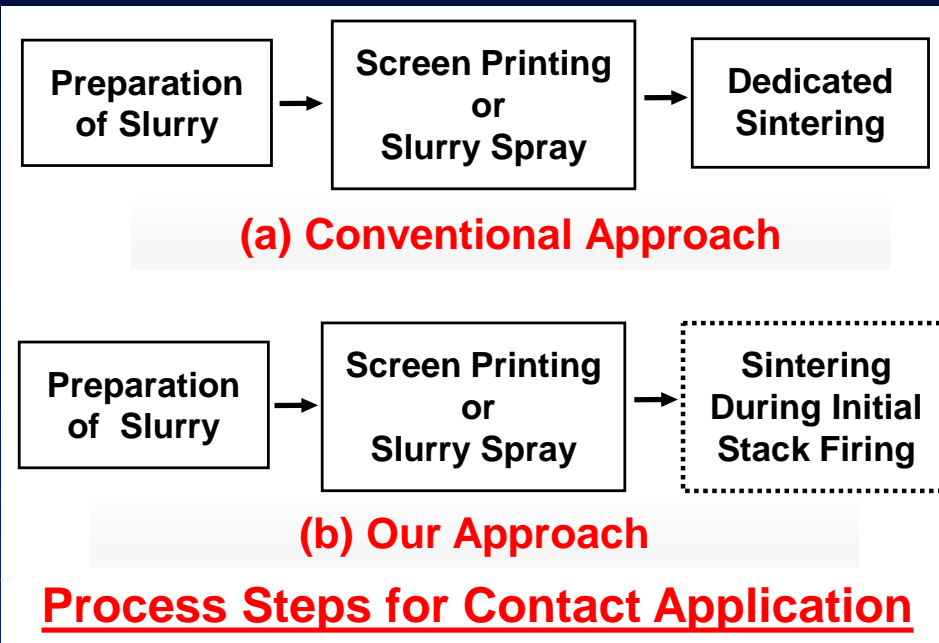
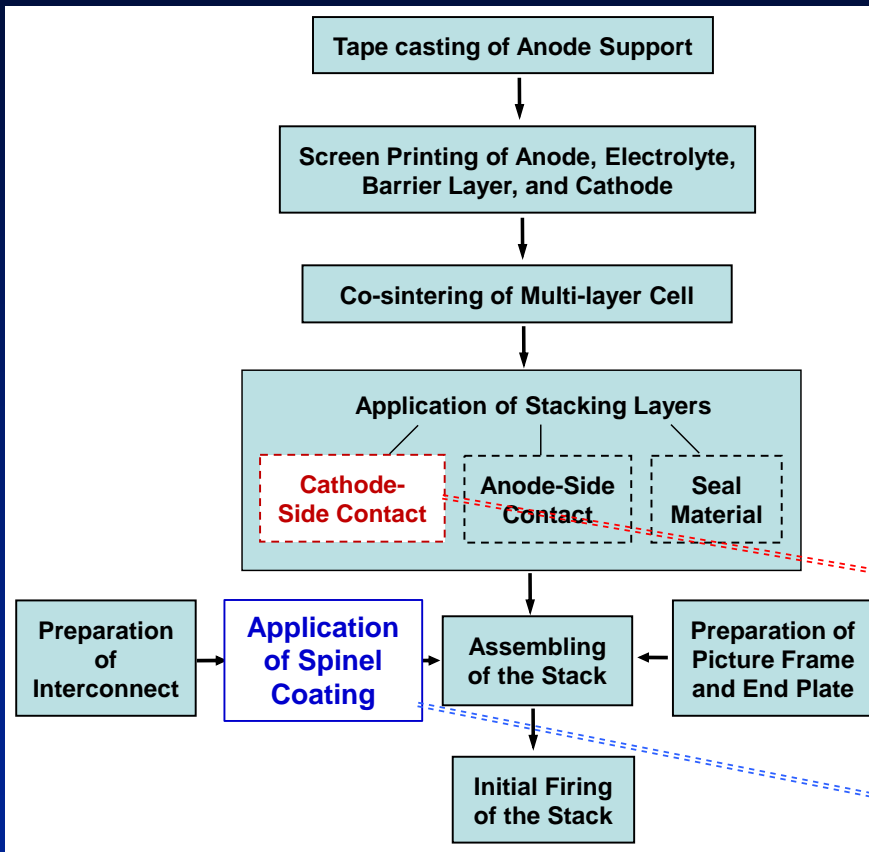
Further Improvement of NiFe_2O_4 -Based Spinel Contact: 2nd-Phase Addition to Form Composite Contact

- The 2nd phase should be electrically conductive, CTE-matched, and chemically compatible with the cathode, interconnect, and $(\text{Ni,Fe})_3\text{O}_4$, and preferably Cr-absorbing.

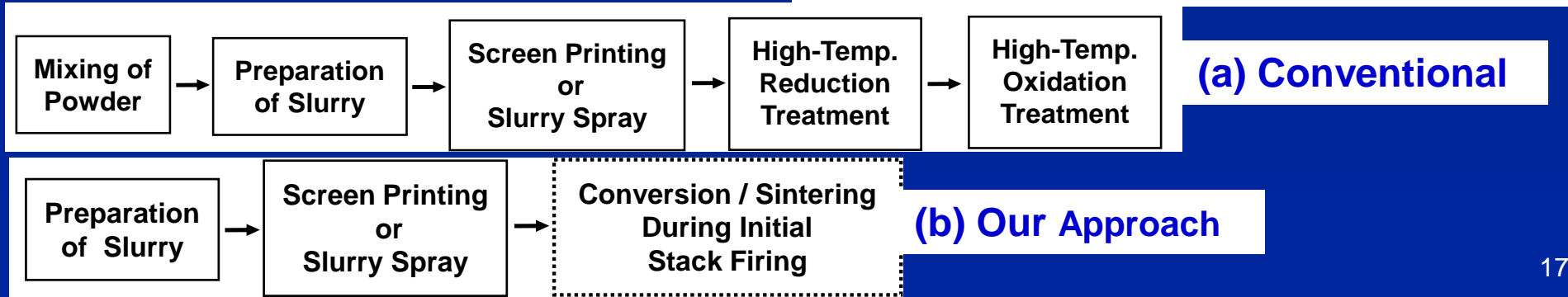
- Potential candidates includes LSM, LSF, LSCF, LSMC, LNF, LCN, etc.
- While NiFe_2O_4 is compatible with Co-free perovskites (LSM/LSF/LNF), a new $(\text{Ni,Co})\text{O}$ phase is formed between the spinel and Co-containing perovskites (LSCF/LSMC/LCF).



Cost Analysis – Simplified Synthesis of Both Contact Layer and Interconnect Coating



Process Steps for Interconnect Coating



Cost Analysis - Production costs of contact layer, interconnect coating, and stack per system

- A stack cost reduction of 6.9% can be achieved, if our new alloy precursor concept is implemented as cathode-side contact.
- An additional 1.1% cost reduction is expected, if interconnect coating can also be synthesized using metallic precursor powder and co-sintering of the interconnect coating/contact layer can be realized during initial stack firing.
- A total stack cost saving of ~8.0% can be achieved, if both of them are considered.

System	Cost	Material Cost (\$)	Annualized Capital and O&M (\$)				Total (\$)	Stack Cost Reduction
			Capital	Electricity	O&M	Labor		
Contact Layer	Conventional	792	769	12	92	225	1,890	6.9%
	New	109	59	6	16	25	215	
Interconnect Coating	Conventional	160	125	55	35	49	424	1.1%
	New	36	59	6	16	25	142	
Stack	Conventional	13,285	7,401	251	1,684	1,806	24,427	8.0%
	New	12,478	6,625	196	1,589	1,582	22,470	

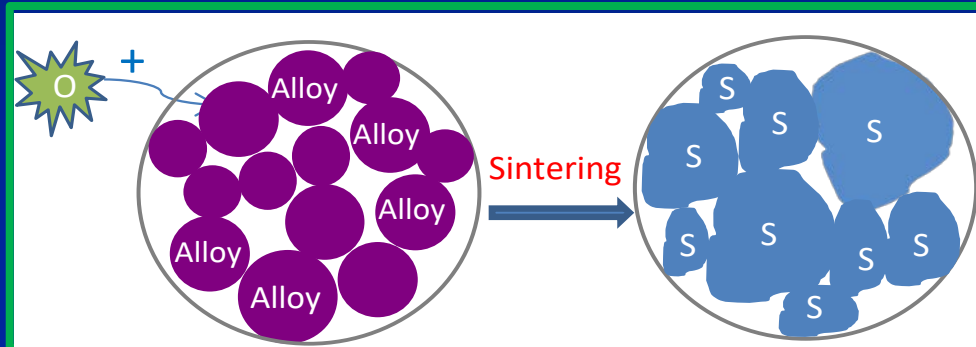
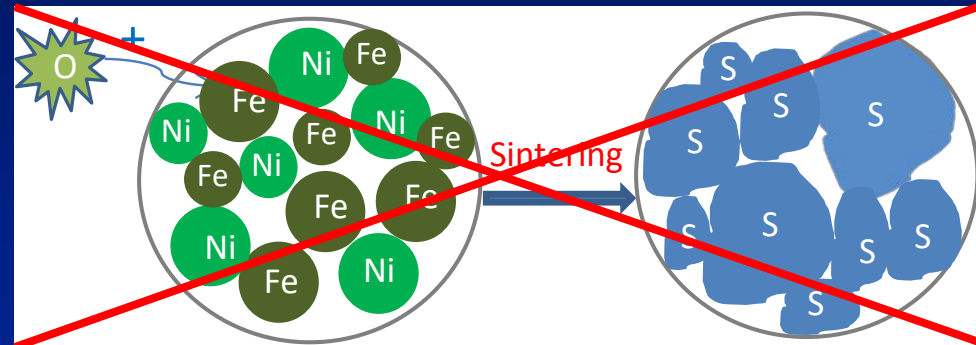
Note: The data for the conventional approach was derived from Weimar et al. (PNNL-22732, 2013); however, instead of Ag, LSM was selected as the contact in the current cost study. 18

Concluding Remarks

- Low-cost, EARS-processed $(\text{Ni,Fe})_3\text{O}_4$ -based layers with promising performance have been successfully synthesized.
- While a mixture of Fe & Ni powders and an Fe-Ni alloy powder can be used as the precursor for the spinel-layer synthesis, the ternary alloy powder derived contact offers the best performance:

- Uniform microstructure
- Low and stable ASR
- Cost advantages

- Only one powder is needed (lower powder process cost)
- No need of powder mixing
- Doped spinel formation via alloy composition adjustment (**multi-component alloys**)



- Multi-component alloy development should be further pursued.

Acknowledgments

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